



# MHD Free Convective Heat and Mass Transfer of a Micropolar Fluid Flow over a Stretching Permeable Sheet with Constant Heat and Mass Flux

E. O. Fatunmbi<sup>1\*</sup> and A. S. Odesola<sup>2</sup>

<sup>1</sup>Department of Mathematics and Statistics, Federal Polytechnic, Ilaro, Ogun State, Nigeria.

<sup>2</sup>Department of Mathematics, University of Lagos, Akoka, Lagos State, Nigeria.

## Authors' contributions

This work was carried out in collaboration between both authors. Author EOF formulated the problem, solved the problem and discuss the findings. Author ASO wrote the introduction and the reviewed the literatures. Both authors read and approved the final manuscript.

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## Abstract

This study investigates heat and mass transfer of chemically reacting and electrically conducting micropolar fluid flow past a vertical stretching permeable sheet in a Darcy-Forchheimer porous medium with constant heat and mass flux and in the presence of heat source/sink. A magnetic field of uniform strength is applied normal to the stretching sheet. The governing partial differential equations governing the flow are transformed into nonlinear coupled ordinary differential equations using appropriate similarity transformations. The resulting equations are solved by shooting method alongside fourth order Runge-Kutta integration scheme. The effects of various flow physical parameters are found on the dimensionless velocity, temperature, concentration and microrotation profiles as well as on the skin friction, wall couple shear stress, Nusselt and Sherwood numbers. It was found that micropolar fluid exhibits a reduction in shear stresses as compared to Newtonian fluids.

Keywords: Stretching sheet; non-Newtonian fluid; magnetohydrodynamic; micropolar fluid.

\*Corresponding author: E-mail: [olusojiephesus@yahoo.com](mailto:olusojiephesus@yahoo.com), [ephesus.fatunmbi@federalpolyilaro.edu.ng](mailto:ephesus.fatunmbi@federalpolyilaro.edu.ng);

## **1 Introduction**

In the recent times, the study of non-Newtonian fluids has attracted the attention of researchers owing to its practical usefulness and applications in industry and engineering processes. The non-Newtonian fluids are fluids which do not obey the linear relationship between the shear stress and the shear rate of the Newton's law, rather, the shear stress and the shear rate are connected in a nonlinear manner. These fluids have real industrial applications, such as in polymer engineering, petroleum drilling, food processing manufacturing and a lot more. It has been observed that the Navier-Stokes equations of classical hydrodynamics can not effectively describe the rheological behaviour of complex fluids of industrial significance. Hence, the development of various kinds of non-Newtonian fluids models depending on different physical characteristics such as Jeffery fluid, Maxwell fluid, Casson fluid, Ostwald de-Wald power law fluid, micropolar fluid a few of many [1].

Eringen [2,3] developed the theory of micropolar fluids and as well derived the constitutive equations for the theory of thermo-micropolar fluids. Micropolar fluids are fluids with dilute suspensions of rigid micro-particles with individual motions that support stress and body moments which constitutes a substantial generalization of the Navier-Stokes model and opens up a new field, of potential applications. Micropolar fluid theory is capable of describing complex rheological behaviour of fluids and provides a good mathematical model for some natural and industrial fluids such as polymeric fluids, biological fluids, particles suspension, animal blood and exotic lubricants which cannot be adequately described by the classical Navier-stokes theory. Its applications in a number of industrial processes, such as extrusion of polymer, the flow of exotic lubricants, colloidal suspensions and the cooling of metallic plate in water bath have also boosted the interest of researchers in studying it [4]. A detailed review, on the theory and applications of micropolar fluids, was given by Lukaszewicz [5] where micropolar fluids were described as having a complex nature and individual fluid particles may be of different shapes and may shrink and/or expand, occasionally changing shapes and rotating independently of the rotational movement of the fluid. The boundary layer flow of such fluids was first studied by Peddieson and McNitt [6] and Wilson [7].

The flow and heat transfer over stretching surfaces has useful and practical applications in engineering activities such as extrusion of plastic sheet, glass blowing, textile and paper production. Similarly, the study of magnetohydrodynamics (MHD) heat and mass transfer over stretching surfaces has found applications in engineering processes such as hot rolling, the extrusion of polymer sheet from a die, the cooling of metallic sheets and a lots more. In such processes, the properties of the final products depend on the kinematic of stretching and the rate of cooling. The rate of cooling can be controlled by drawing the sheets in an electrically conducting fluid subjected to a magnetic field. Crane [8], pioneered work on stretching sheet, Gupta and Gupta [9] extended the work to include heat and mass transfer on stretching sheet with suction or blowing. Many other researchers [10-12] have also investigated fluid flows past stretching surfaces.

The study of heat and mass transfer analysis with chemical reaction, heat generation/absorption in the boundary layer flow is of practical importance due their importance in chemical processes and hydrometallurgical industries, for instance, food processing, manufacturing of ceramics and polymer production [13,14]. Heat generation/absorption influence may change the temperature distribution of the fluid flow and in consequence affect various engineering devices. To this end, Krishna and Reddy [15] discussed the unsteady MHD free convection in a boundary layer flow of an electrically conducting fluid through porous medium subject to uniform transverse magnetic field over a moving infinite vertical plate in the presence of heat source and chemical reaction. Krishna and Kamboji, [16] have investigated the simulation on the MHD forced convective flow through stumpy permeable porous medium (oil sands, sand) using Lattice Boltzmann method. Krishna and Jyothi [17] examined the Hall effects on MHD Rotating flow of a visco-elastic fluid through a porous medium over an infinite oscillating porous plate with heat source and chemical reaction. Similarly, Srinivasacharya and Mendu [18] studied free convection in MHD micropolar fluid with radiation and chemical reaction effects. Bhattacharyya and Layek [19] studied MHD boundary layer flow with diffusion and chemical reaction over a porous flat plate with suction/blowing. Mohammed and Abo-Dahab [20] examined heat and mass transfer in MHD micropolar flow over a vertical moving porous plate in a porous medium with heat generation using perturbation technique.

The flow and heat transfer of MHD micropolar fluids in porous surfaces under the influence of a magnetic field has also been investigated by researchers owing to its applications in engineering devices such as MHD generators, geothermal energy extractions, nuclear reactors/burial of nuclear wastes and boundary layer control in the field of aerodynamics [21]. In view of this, Reddy et al. [22] investigated MHD flow of viscous incompressible nano-fluid through a saturating porous medium. Fatunmbi and Adeniyani [23] investigated MHD stagnation point flow of micropolar fluid past permeable stretching plate in porous media with thermal radiation and chemical reaction.

Thermal radiation effects become important when there is occurrence of high temperature difference between the surface temperature and the ambient temperature and such study is found useful in building relevant equipments and appliances in engineering operations such as in nuclear reactors, electric power generation and solar power technology. Boetcher et al. [24] examined numerical simulation of the radiative heating of a moving sheet, Mukhopadhyay [25] studied effects of thermal radiation and variable fluid viscosity on stagnation point flow past a porous stretching sheet.

The aim of the present work is to investigate free convection heat and mass transfer of an electrically conducting non-Newtonian micropolar fluid flow over a stretching permeable sheet with constant heat and mass flux in a saturated Darcy-Forchheimer porous medium. The influences of radiation, viscous dissipation, heat source and chemical reaction are also considered. The system of partial differential equations governing the fluid flow is transformed into coupled nonlinear ordinary equations by similarity transformations and the resulting equations are numerically solved by shooting method alongside fourth order Runge-Kutta method.

## 2 Formulation of the Problem

Consider a steady, two dimensional flow of viscous, incompressible free convective, electrically and thermally radiating and electrically conducting micropolar fluid over a stretching permeable plate in a saturated Darcy-Forchheimer porous medium. A uniform magnetic field of strength  $B_o$  is applied normal to the direction of flow in which  $(x, y)$  describes the stretching and the transverse coordinates with corresponding velocity component  $(u, v)$ . The constant heat flux  $(-k \frac{\partial T}{\partial y}) = A$ , the constant mass flux  $(-Dm \frac{\partial c}{\partial y}) = B$  are considered and the uniform plate temperature  $T_w > T_\infty$ , where  $T_\infty$  is the free stream temperature. The fluid stretching velocity  $u_w$  is assumed to vary proportional to the distance  $x$  i.e.  $u_w = ax$ , where  $a$  is positive constant. All the fluid properties are isotropic and constant except the density variation with temperature and concentration in the body force term which is approximated by Boussinesq approximation. It is assumed also that the magnetic Reynolds number is small such that the induced magnetic field is neglected as compared to the applied magnetic field. In addition, the fluid is taken to be gray emitting and absorbing but not scattering, the optically thick radiative flux is simplified using the Rosseland approximation.

Under the above assumptions, the boundary layer and invoking the Boussinesq approximations, the governing equations of continuity, momentum, microrotation, energy and concentration of the fluid flow are respectively given as:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \frac{(\mu + \kappa)}{\rho} \frac{\partial^2 u}{\partial y^2} + \frac{\kappa}{\rho} \frac{\partial N}{\partial y} + g\beta_T(T - T_\infty) + g\beta_c(C - C_\infty) - \frac{\sigma B_0^2}{\rho} u - \frac{v}{K_p} u - \frac{F}{K_p} u^2, \quad (2)$$

$$u \frac{\partial N}{\partial x} + v \frac{\partial N}{\partial y} = \frac{\gamma}{\rho j} \frac{\partial^2 N}{\partial y^2} - \frac{\kappa}{\rho j} \left( 2N + \frac{\partial u}{\partial y} \right), \quad (3)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \frac{k}{\rho C_p} \frac{\partial^2 T}{\partial y^2} + \frac{(\mu + \kappa)}{\rho C_p} \left( \frac{\partial u}{\partial y} \right)^2 - \frac{1}{\rho C_p} \frac{\partial q_r}{\partial y} + \frac{q}{\rho C_p} (T - T_\infty) + \frac{D_m K_T}{C_s C_p} \frac{\partial^2 C}{\partial y^2}, \quad (4)$$

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = Dm \frac{\partial^2 C}{\partial y^2} + \frac{D_m k_T}{T_m} \frac{\partial^2 T}{\partial y^2} - k_r (C - C_\infty). \quad (5)$$

The boundary conditions are as follows:

$$\begin{aligned} u = u_w = ax, v = v_w, N = -m \frac{\partial u}{\partial y}, -k \frac{\partial T}{\partial y} = A, -Dm \frac{\partial C}{\partial y} = B \text{ at } y = 0, \\ u \rightarrow 0, N \rightarrow 0, T \rightarrow T_\infty, C \rightarrow C_\infty \text{ as } y \rightarrow \infty. \end{aligned} \quad (6)$$

Here,  $\mu, \nu, \rho, \kappa, j, \gamma$  and  $v_w$ , are dynamic viscosity, kinematic viscosity, fluid density, vortex viscosity, micro inertial per unit mass, spin gradient viscosity and suction/injection term. Similarly,  $T, C, N, k, B_0$  and  $K_p$  are the fluid temperature, fluid concentration, component of microrotation vector normal to  $xy$  plane, thermal conductivity, magnetic field intensity and permeability of the porous medium. Others are:  $k_r, \sigma, C_p, T_\infty, C_\infty, T_m, Dm, q, A, B$  and  $q_r$  represent rate of chemical reaction, electrical conductivity, specific heat at constant pressure, free stream temperature, and the free stream concentration, mean fluid temperature, molecular diffusivity, volumetric rate of heat generation, constant heat flux per unit area, coefficient of mass flux per unit area and radiative heat flux respectively  $F = F_0 x^{-1}, \beta_T = \beta_0 x^{-1}, \beta_c = \beta_0^* x^{-1}$  represent Forchheimer constant, coefficient of thermal expansion, coefficient of volumetric expansion, and  $F_0, \beta_0$  and  $\beta_0^*$  are constants (see Makinde [26]).

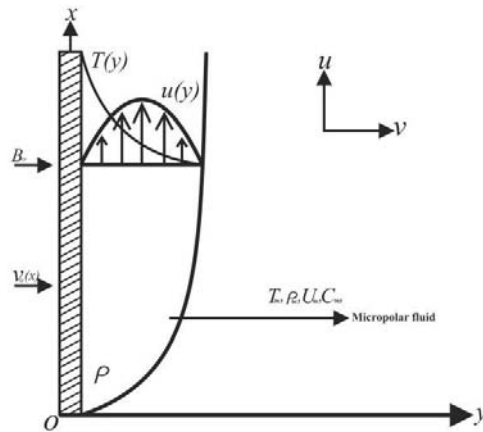


Fig. 1. Physical model and coordinate system

Also,  $m$  is a surface boundary parameter with  $0 \leq m \leq 1$ . The case when  $m = 0$  corresponds to  $N = 0$ , this represents a strong concentration such that the micro-particles close to the wall are unable to rotate.

When  $m = \frac{1}{2}$ , this indicates weak concentration of micro-particles and the vanishing of anti-symmetric part of the stress tensor and the case when  $m = 1$  is used for modelling turbulent boundary layer flows (see Peddieson [27], Ahmadi [28], Jena and Mathur [29]).

$\gamma = \left( \mu + \frac{\kappa}{2} \right) j$ , is the spin gradient viscosity. This assumption has been invoked to allow the field of equations to predict the correct behaviour in the limiting case when the microstructure effects becomes negligible and the total spin  $N$  reduces to the angular velocity [28].

Using Rosseland approximation,

$$q_r = -\frac{4\sigma^*}{3\alpha^*} \frac{\partial T^4}{\partial y}, \quad (7)$$

is the radiative heat flux [30].

where,  $\alpha^*$  is the mean absorption coefficient and  $\sigma^*$  is the Stefan-Boltzman constant. We suppose that there exists sufficiently small temperature difference within the flow, such that  $T^4$  can be expressed as a linear combination of the temperature. Expanding  $T^4$  in Taylor series about  $T_\infty$  to obtain

$$T^4 \approx 4T_\infty^3 T - 3T_\infty^4. \quad (8)$$

Hence,

$$\frac{\partial q_r}{\partial y} = -\frac{16\sigma^* T_\infty^3}{3\alpha^*} \frac{\partial T^2}{\partial y^2} \quad (9)$$

Introducing the stream function

$\psi(x, y)$  as  $u = \frac{\partial \psi}{\partial y}$ ,  $v = -\frac{\partial \psi}{\partial x}$ , equation (1) is automatically satisfied.

The following dimensionless variables are substituted into Eqs. (2-6)

$$\begin{aligned} \psi(x, y) &= xf(\eta)(av)^{\frac{1}{2}}, \eta = \left(\frac{a}{v}\right)^{\frac{1}{2}}, N = xg(\eta) \sqrt{\left(\frac{a^3}{v}\right)}, \\ \theta(\eta) &= \frac{k(T-T_\infty)}{A} \left(\frac{a}{v}\right)^{\frac{1}{2}}, \phi(\eta) = \frac{Dm(C-C_\infty)}{B} \left(\frac{a}{v}\right)^{\frac{1}{2}}. \end{aligned} \quad (10)$$

The resulting non-linear ODEs are:

$$(1 + K)f''' + ff'' + \lambda^2 + Kg' - (Da + M)f' - (Fs + 1)f'^2 = 0 \quad (11)$$

$$\lambda g'' + fg' - f'g - 2Hg - Hf'' = 0 \quad (12)$$

$$(1 + 4R/3)\theta'' + PrEc(1 + K)f''^2 + Prf\theta' + PrQ\theta + PrDu\phi'' = 0 \quad (13)$$

$$\phi'' + Scf\phi' + ScSr\theta'' - Sc\gamma_1\phi = 0 \quad (14)$$

The boundary conditions are:

$$\eta = 0: f' = 1, f = fw, g = -mf'', \theta' = -1, \phi' = -1, \quad (15)$$

$$\eta \rightarrow \infty: f' = \lambda, g \rightarrow 0, \theta \rightarrow 0, \phi \rightarrow 0. \quad (16)$$

Here, prime denotes differentiation with respect to  $\eta$ ,  $K = \frac{\kappa}{\mu}$  is the material parameter,  $fw = -\frac{v_w}{\sqrt{av}}$

with  $fw > 0$  as the suction and  $fw < 0$  corresponds to injection.  $Da = \frac{v}{aK_p}$  is the Darcy parameter,

$M = \frac{\sigma B_o^2}{a\rho}$  is the Magnetic parameter,  $Pr = \frac{\mu Cp}{k}$  is the Prandtl number,  $Sc = \frac{v}{Dm}$  is the Schmidt

number,  $Q = \frac{q}{a\rho Cp}$  is the heat generation/absorption parameter,  $Fs = \frac{F_0}{K_p}$  is the Forchheimer number,

$Gr = g\beta_0\sqrt{\frac{v}{a^5}}$  is the thermal Grashof number,  $Gc = g\beta_0^*\sqrt{\frac{v}{a^5}}$  is the solutal Grashof number,

$\lambda = \frac{\gamma}{\nu\rho j}$  is the spin gradient viscosity parameter,  $H = \frac{\kappa}{a\rho j}$  is the vortex viscosity parameter,

$Ec = \frac{u^3 k}{Ax Cp \sqrt{av}}$  is the Eckert number,  $R = \frac{4\sigma^* T_\infty^3}{\alpha^* k_\infty}$  is the radiation parameter,  $Du = \frac{BK_T}{\nu Cs Cp A} \frac{k}{A}$  is

the Dufour number,  $Sr = \frac{DmK_T}{BT_m} \frac{B}{k}$  is the Soret number and  $\gamma_1 = \frac{k_r}{a}$  is the chemical reaction parameter.

## 2.1 Quantities of physical interest

The physical quantities of interest are the non-dimensional skin friction coefficient, the wall couple stress, the Nusselt number and the Sherwood number. These are respectively defined as :

$$C_f = \frac{\tau_w}{\rho u_w^2} = [1 + K(1 - m)f''(0)]Re_x^{-\frac{1}{2}} \quad (17)$$

$$M_w = \left(\gamma \frac{\partial N}{\partial y}\right)_{y=0} = \mu u_w \left(1 + \frac{K}{2}\right) g'(0) \quad (18)$$

$$Nu_x = \frac{x A}{k(T_w - T_\infty)} = \frac{Re_x^{\frac{1}{2}}}{\theta(0)} \quad (19)$$

$$Sh_x = \frac{x B}{Dm(C_w - C_\infty)} = \frac{Re_x^{\frac{1}{2}}}{\phi(0)} \quad (20)$$

where  $\tau_w = \left[ \mu + \kappa \frac{\partial u}{\partial y} + \kappa N \right]_{y=0}$  is the surface shear stress,  $u_w = ax$  is the characteristics velocity ,  
 $Re_w = \frac{u_w x}{\nu}$  is the local Reynolds number,  $A$  and  $B$  are respectively given as  $A = -k \left( \frac{\partial T}{\partial y} \right)_{y=0}$ ,  $B = -Dm \left( \frac{\partial c}{\partial y} \right)_{y=0}$

### 3 Method of Solution

The system of non-linear ordinary differential equations (11 – 14 ) with the boundary conditions (15 – 16) were solved numerically using Fourth order Runge-Kutta integration scheme alongside shooting method. Systematic estimate of  $f''(0)$  and  $\theta(0)$  were carried out with shooting technique until the boundary conditions at infinity decay exponentially to zero. The iteration process is repeated until the convergence criterion for all the variables at  $10^{-8}$  is achieved. The step size  $\nabla \eta = 0.001$  is used for the numerical solution and the boundary condition  $\eta \rightarrow \infty$  is approximated by  $\eta_{max} = 10$ .

### 4 Results and Discussion

To have a clear insight into the behaviour of each of the flow parameters on the physical problem, the computational analysis are carried out for the dimensionless velocity, temperature, concentration and microrotation. The default values of the computation are as follows:

$M = 0.5$ ,  $K = 0.5$ ,  $Ec = 0.01$ ,  $Pr = 0.71$ ,  $Sc = 0.22$ ,  $R = 0.2$ ,  $\lambda = 2$ ,  $Da = 0.5$ ,  $Fs = 0.5$ ,  $Q = 0.5$ ,  $m = 0.5$ , and  $fw = 0.5$ ,  $Sr = 1$ ,  $Du = 0.2$ ,  $Gr = 4$ ,  $Gc = 2$ . The plotted graphs correspond to these values unless otherwise indicated on the graph.

To authenticate our numerical analysis, a comparison of the values of the surface temperature  $\theta(0)$  for various values of Prandtl number  $Pr$  has been made with existing work in literature under some limiting cases and found to be in excellent agreement as shown in Table 1.

Table 2 shows the numerical values of skin friction coefficient, Nusselt number, Sherwood number and the wall couple stress for some pertinent parameters. From this table, it is seen that the material parameter  $K$ , the Magnetic parameter  $M$  and Forchheimer parameter  $Fs$  cause a reduction in the skin friction coefficient, Nusselt number, Sherwood number and the wall couple stress. On the other hand, the skin friction coefficient, wall couple stress and the sherwood number increase with heat generation parameter  $Q$  and Dufour parameter  $Du$ .

Figs. 2-3 respectively describe the impact of magnetic field parameter  $M$  on the velocity and temperature profiles. Observation from Fig. 2 reveals that the fluid velocity and the velocity boundary layer thickness decrease with an increase in the value of the magnetic field parameter  $M$ . This physical response shows that the application of the transverse magnetic field in an electrically conducting fluid creates a retarding force known as Lorentz force which acts against the fluid motion and slows it down. In consequence, the micropolar fluid temperature increases as shown in Fig. 3. Fig. 4 shows the variation of the dimensionless velocity with  $\eta$  for various values of material (micropolar) parameter  $K$ . It is noticed that the velocity profiles decrease very close to the plate with the velocity of viscous fluid  $K = 0$  higher than that of micropolar fluid. However, further away from the plate the fluid velocity increases with an increase in  $K$  due to the rising in the momentum boundary layer thickness. In such case, the micropolar fluid velocity is

higher than that of viscous fluid ( $K = 0$ ). Fig. 5 shows that the microrotation profiles rises near the plate and it is negative. The negative values of the microrotation indicate a reverse spinning of the micro-particles.

**Table 1. Comparison of the values of surface temperature  $\theta(0)$  with existing works for different values of  $Pr$  when  $K = M = R = Da = Fs = Ec = Q = Sc = Du = Sr = \gamma_1 = H = 0$**

$Pr$	Salleh et al. [31]	Qasim et al. [12]	Present results
0.72	-	2.15916	2.15707
1.00	1.71816	1.71816	1.71818
3.00	0.85819	0.85819	0.85819
5.00	0.63773	0.63773	0.63773
7.00	0.52759	0.52758	0.52759
10.00	0.43327	0.43327	0.43328
100.00	0.12877	0.12877	0.12877

**Table 2. Values of  $f''(0)$ ,  $\frac{1}{\theta(0)}$ ,  $\frac{1}{\phi(0)}$  and  $g'(0)$  for variations in  $K, M, Fs, Q, fw, Du$  and  $\gamma_1$**

K	M	Fs	Q	$f_w$	$Du$	$\gamma_1$	$f''(0)$	$1/\theta(0)$	$1/\phi(0)$	$g'(0)$
0.00							1.602837	0.539383	1.071818	1.088777
0.75	0.5	0.5	0.5	0.2	0.5	0.2	1.148439	0.537536	1.069651	0.987890
2.00							0.900419	0.532433	1.064202	0.781472
0.5	0.00						1.767453	0.554924	1.084236	1.198142
	1.50						1.310287	0.510971	1.050286	0.895471
	3.5						0.832752	0.462838	1.017619	0.591926
	0.5	0.5					2.309064	0.414462	1.095415	1.395224
		1.5					1.973539	0.386096	1.081265	1.181854
		2.5					1.711728	0.363254	1.072580	1.020244
			0.1				1.089493	0.681017	0.975858	0.754021
			0.35				1.382569	0.592628	1.029425	0.942556
			0.75				2.062246	0.452645	1.167758	1.399672
			0.5	-0.5			3.083214	0.315423	1.177637	1.692487
				-0.2			2.609241	0.371884	1.114698	1.514225
				0.2			2.019750	0.461203	1.080304	1.274631
					0.2		1.602837	0.539384	1.0718180	1.087776
					1.0		2.520743	0.377711	1.2952781	1.720463
					0.5	0.5	1.602837	0.538394	1.0718182	1.087776
						1.0	1.568575	0.535830	1.0718185	1.065148

Figs. 6-7 describe the influence of Forchheimer  $Fs$  on velocity and temperature profiles. As Forchheimer  $Fs$  increases, the velocity distribution in the boundary layers decreases due to the tightness of the porous medium, also the hydrodynamic boundary layer thickness decreases as shown in Fig.7, a similar effect happens in the case of the Darcy parameter  $Da$ . The resistance to the fluid motion created by the porous medium causes the fluid to heat up leading to a rise in thermal boundary layer thickness and as a result the temperature rises as depicted in Fig. 7. Fig. 8 displays the effect of the radiation parameter  $R$  on the temperature distributions. Observation shows that an increase in  $R$  has the tendency to enhance the conduction effect and increase temperature at every point away from the surface, in terms of the boundary layer, the thickness of the thermal boundary layer rises as  $R$  increases. Hence, to have the cooling at a faster rate  $R$  should be reduced. Fig. 9. is a plot of temperature against  $\eta$  for different values of heat generation parameter  $Q$ . Heat generation enhances temperature distribution across the boundary layer.



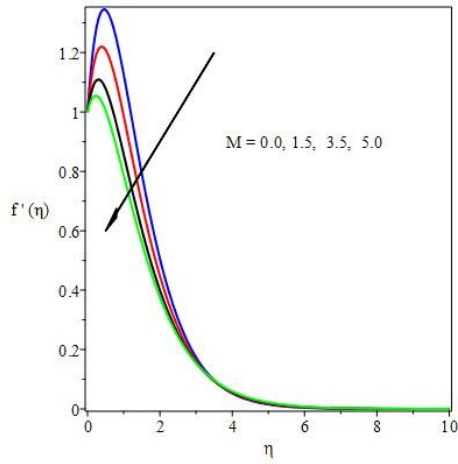


Fig. 2. Effect of  $M$  on Velocity profiles

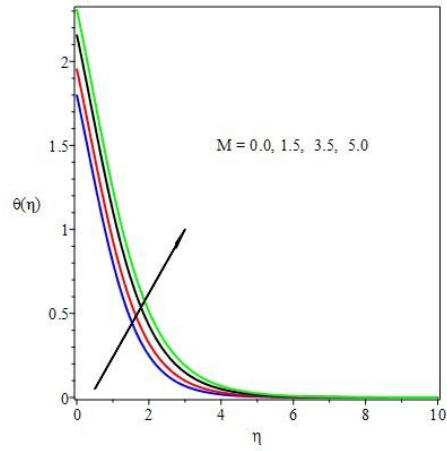


Fig. 3. Effect of  $M$  on Temperature

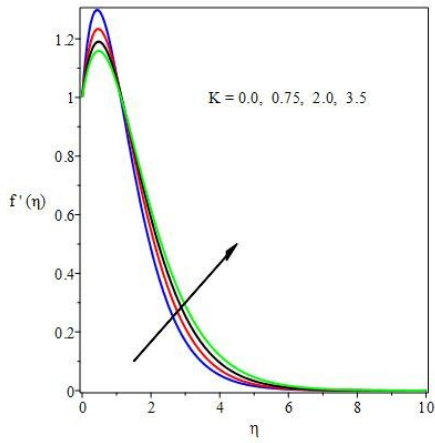


Fig. 4. Effect of  $K$  on Velocity

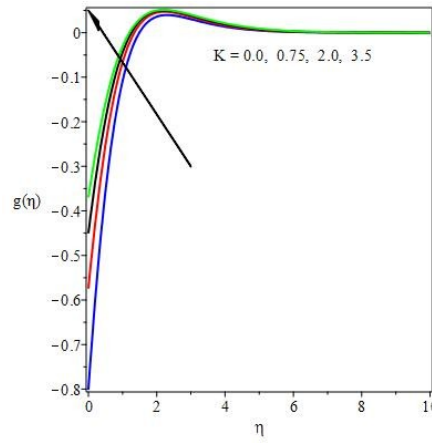


Fig. 5. Effect of  $K$  on Microrotation profiles

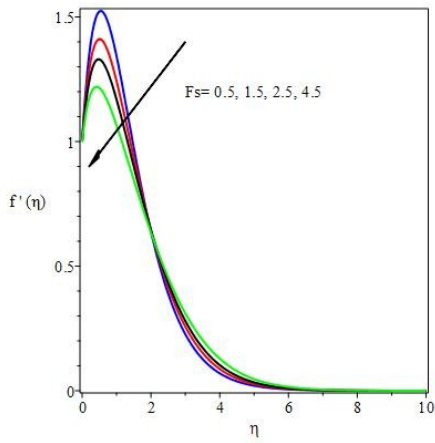


Fig. 6. Effect of  $F_s$  on Velocity profiles

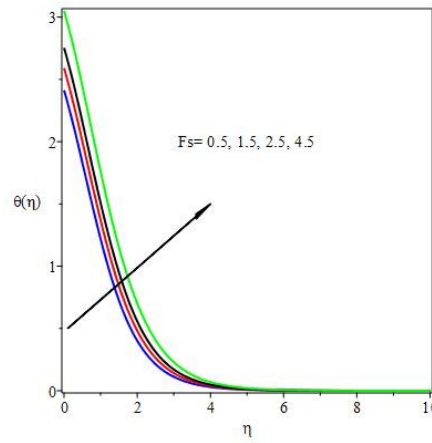
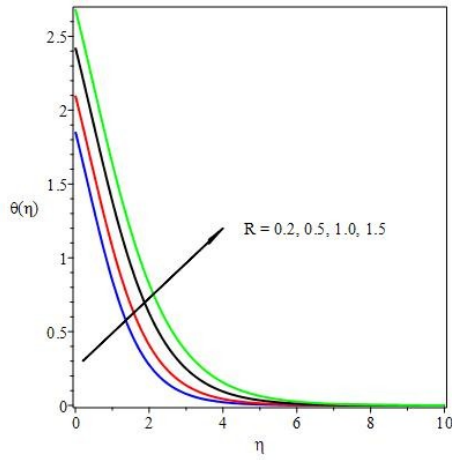
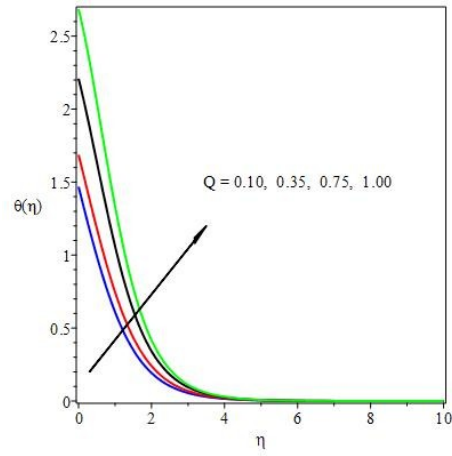


Fig. 7. Effect of  $F_s$  on Temperature profiles



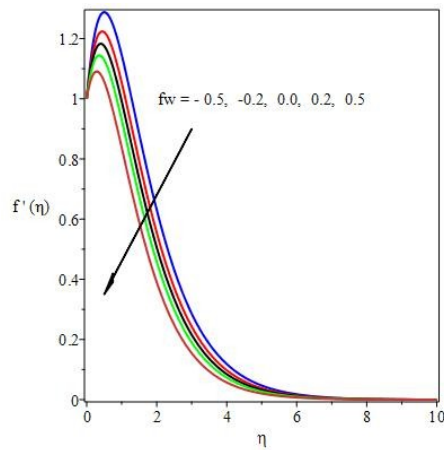
**Fig. 8. Effect of  $R$  on Temperature**



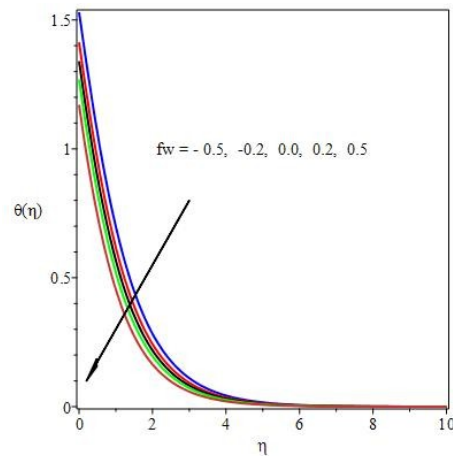
**Fig. 9. Effect of  $R$  on Temperature profiles**

Figs. 10-11 display the influence of suction/injection  $f_w$  on velocity and temperature distributions across the boundary layer. Observation shows that both the hydrodynamic and thermal boundary layers fall with an increase in the suction velocity ( $f_w > 0$ ). In addition, suction produces a damping effect on the fluid flow due to the fact that the heated fluid is being pushed towards the plate such that the buoyancy force acted to resist the fluid as a result of high influence of viscosity. On the other hand, an increase in the injection parameter  $f_w < 0$  enhances velocity distribution within the boundary layer.

Fig. 12 depicts a decrease in the microrotation profiles and a negative rotation of the micro-particles with an increase in the spin gradient viscosity parameter  $\lambda$ . However, when the surface boundary parameter  $m = 0$  a case of strong concentration of micro-elements, the microrotation decreases near the plate while it increases further away from the plate and with positive spinning of micro-constituents as demonstrated in Fig. 13.



**Fig. 10. Effect of  $f_w$  on Velocity profiles**



**Fig. 11 Effect of  $f_w$  on Temperature**

Fig. 14 shows the influence of vortex viscosity parameter  $H$  on the microrotation profiles. There is a rise in the microrotation profiles and a negative rotation of the micro-particles with an increase in the vortex viscosity parameter  $H$ . Fig. 15 illustrates the effect of Prandtl number  $Pr$  on the temperature profiles. It is

evident that increase in the Prandtl number  $Pr$  causes a reduction in the temperature profile. An increase in  $Pr$  implies reducing thermal boundary layer thickness which in turn lowers the average temperature within the boundary layer. Prandtl parameter  $Pr$  can therefore be applied to enhance the rate of cooling as fluids with lower  $Pr$  produce higher conductivities and at such heat diffuses speedily away from the heated plate than for higher values of  $Pr$ .

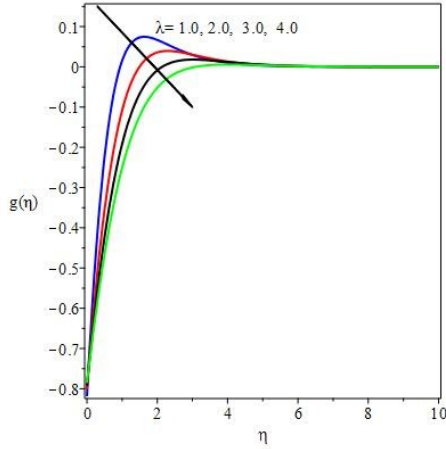


Fig. 12. Effect of  $\lambda$  on Microrotation

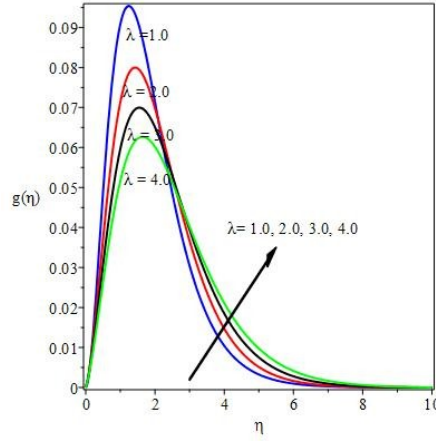


Fig. 13. Effect of  $\lambda$  on Microrotation @  $m=0$

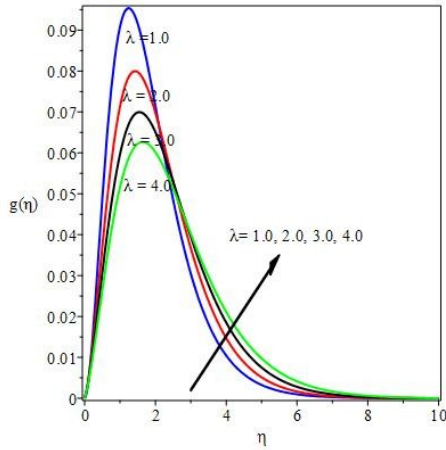


Fig. 14. Effect of  $H$  on Microrotation

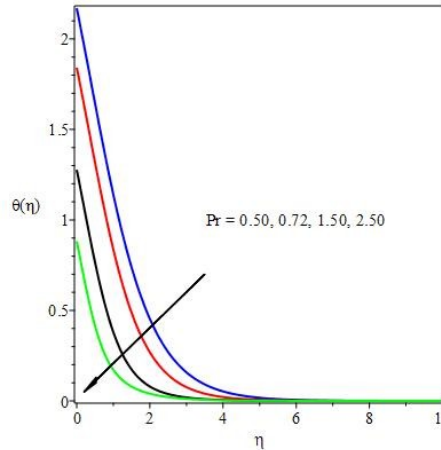


Fig. 15 Effect of  $Pr$  on Temperature

Figs. 16 and 17 portray the effect of the destructive chemical reaction parameter  $\gamma_1 > 0$  and the generative chemical reaction parameter  $\gamma_1 < 0$  on the concentration profiles. A rise in destructive chemical reaction parameter ( $\gamma_1 > 0$ ) causes a decrease in concentration of the micropolar fluid along the wall of the surface due to the reduction in the solutal boundary layer thickness as depicted in Fig. 16. However, the trend is reversed for the generative reaction ( $\gamma_1 < 0$ ) as shown in Fig. 17. Furthermore, it is noticed that the magnitude of generative chemical reaction ( $\gamma_1 < 0$ ) is higher than that of destructive chemical reaction ( $\gamma_1 > 0$ ) because  $\gamma_1 > 0$  occurs with much disturbances than  $\gamma_1 < 0$ , for this reason, molecular motion in

the case of  $\gamma_1 > 0$  is much greater leading to an increase in mass transport phenomenon. Fig. 18 reveals that an increase in Schmidt number  $Sc$  dampens the solutal boundary layer thickness. Physically, Schmidt number  $Sc$  represents the ratio of the momentum diffusivity to the mass (species) diffusivity  $Dm$  and depicts the relative thickness of the hydrodynamic boundary layer and concentration boundary layer. Fig. 19 describes the effect of Soret Number  $Sr$  on the concentration profiles. An increase in Soret number produces an increase in the concentration distributions and enhance the solutal boundary layers thickness.

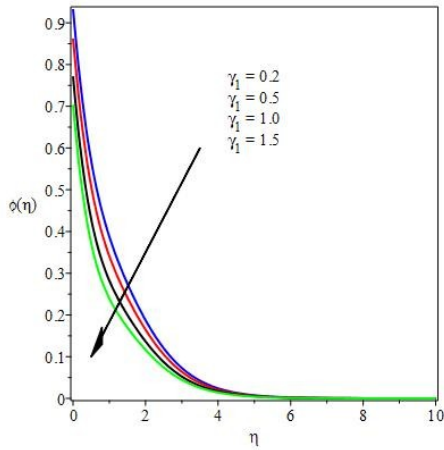


Fig. 16. Effect of  $\gamma_1$  on Concentration

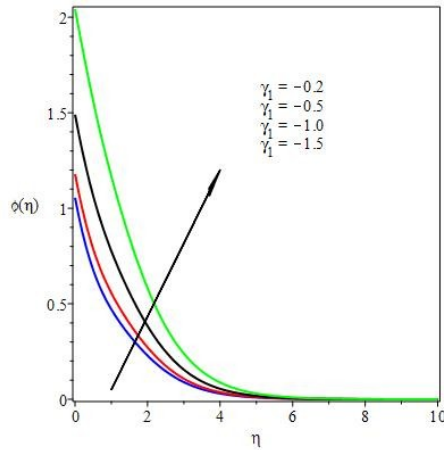


Fig. 17. Effect of  $\gamma_1$  on Concentration profiles

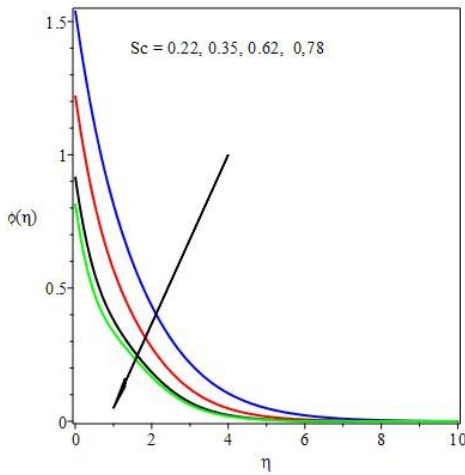


Fig. 18. Effect of  $Sc$  on Concentration

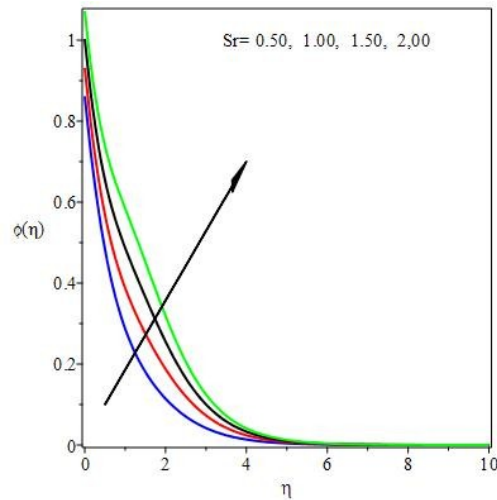


Fig. 19. Effect of  $Sr$  on Concentration

## 5 Conclusion

This paper considers the free convective boundary layer flow, heat and mass transfer of an electrically conducting micropolar fluid past a linearly stretching sheet in a saturated Darcy-Forchheimer porous medium with constant heat and mass flux. The governing partial differential equations of the fluid flow are transformed into non-linear coupled ordinary differential equations using an appropriate similarity variables and the resulting equations are solved with the fourth order Runge-Kutta integration scheme coupled with

shooting method. Comparison of the present results are made with existing work in the literature under some limiting cases and found to be in excellent agreement.

The main observations are:

- An increase in the material (micropolar) parameter  $K$  causes a reduction in the skin friction coefficient  $f''(0)$ , heat transfer  $\theta'(0)$ , mass transfer  $\phi'(0)$  and the wall couple stress  $g'(0)$ . Thus, the inclusion of micropolar fluid is to reduce the drag along the plate.
- The material (micropolar) parameter  $K$  causes a decrease in the fluid velocity close to the plate but increase in fluid velocity further away from the plate, also, an increase in  $K$  causes a rise in the microrotation profiles. .
- The heat transfer coefficient increases with increase in suction parameter  $f_w$  as the skin friction coefficient rises with the Dufour effect.
- The species concentration reduces with an increase in the destructive chemical reaction parameter  $\gamma_1 > 0$  parameter, Soret  $Sr$  and Schmidt numbers  $Sc$  while the trend is reversed for the generative chemical reaction  $\gamma_1 < 0$  parameter.
- The momentum boundary layer thickness reduces with an increase in the Darcy  $Da$  and Forchheimer  $FS$  parameters while the opposite is the case for thermal boundary layer thickness.
- The thermal boundary layer thickness diminishes with an increase in  $Pr$  while the opposite trend is observed with an increase in the radiation parameter  $R$  and heat generation parameter  $Q$ .

## Competing Interests

Authors have declared that no competing interests exist.

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